

Eddy Covariance Experiment Applications, Design, and Site Selection

Liukang Xu

Aug 24, 2020



Topics will be covered

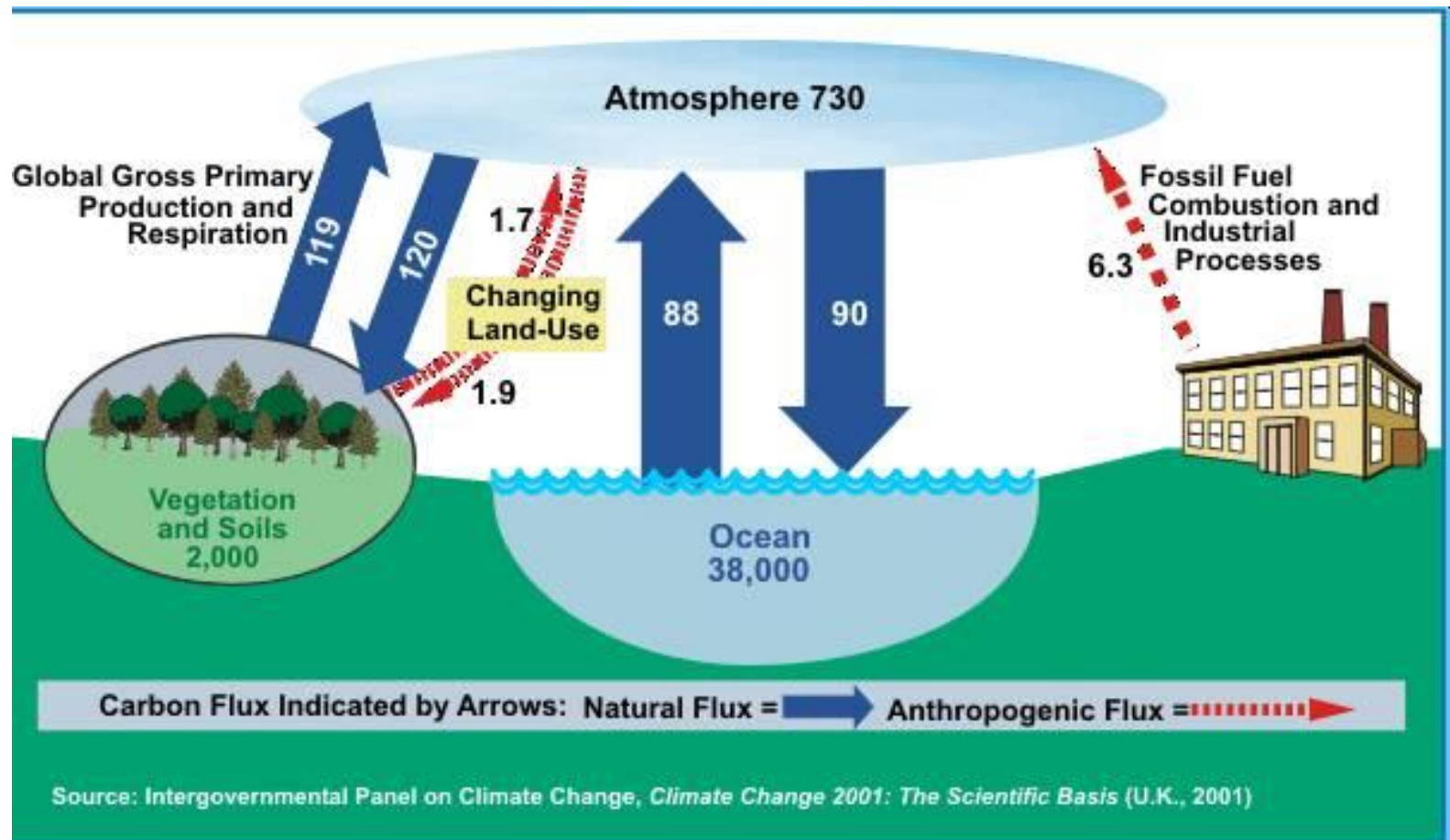
1. Eddy covariance applications
2. Concept of flux footprint and fetch requirement
3. Designing and implementation of EC experiment
 - Tower height
 - Location of the tower

Applications

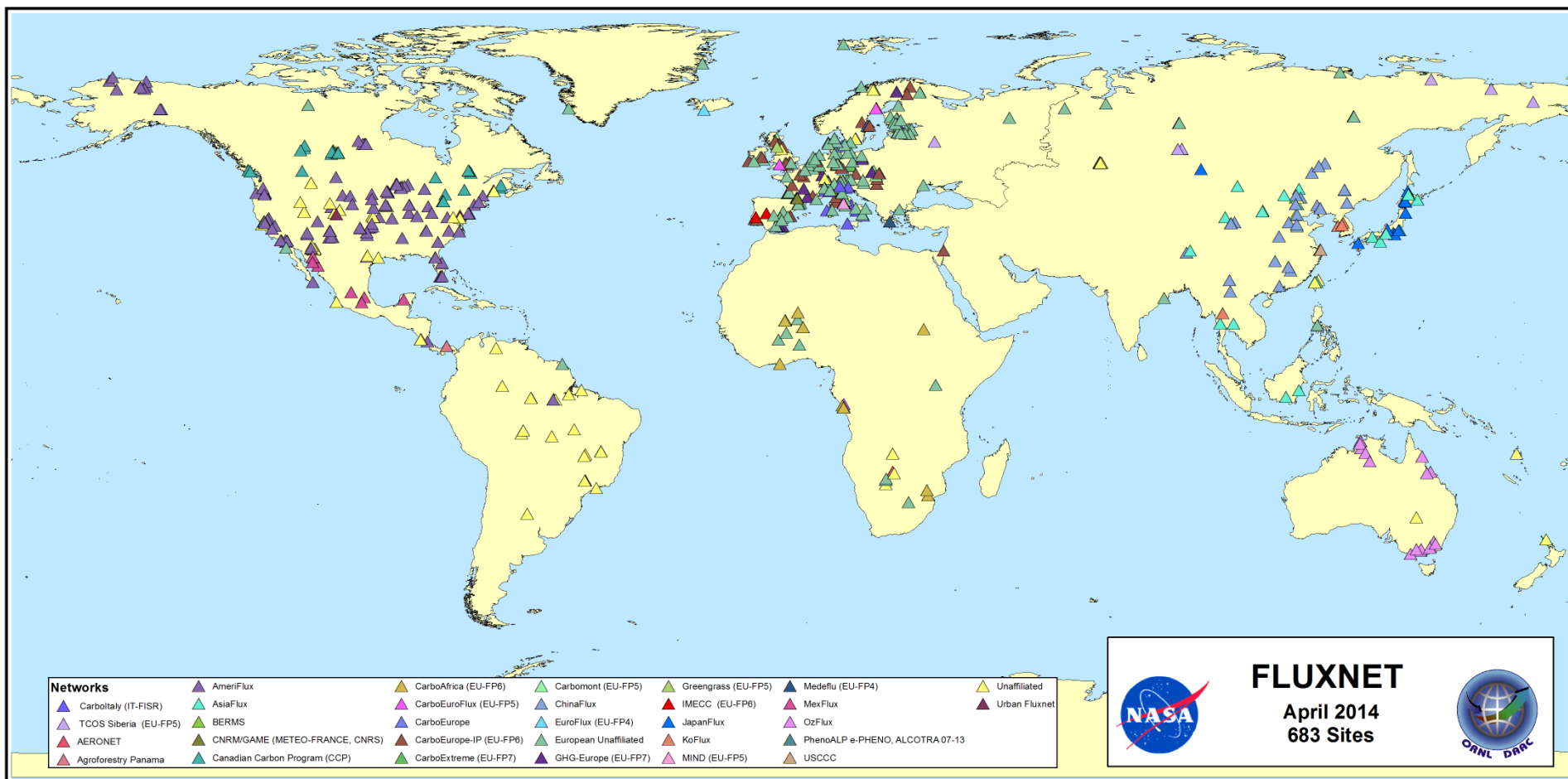
- Climate change research
Global Carbon Cycle
- Agricultural applications
Other GHG fluxes, N_2O , CH_4 , $^{13}\text{CO}_2$ etc
- Industrial applications



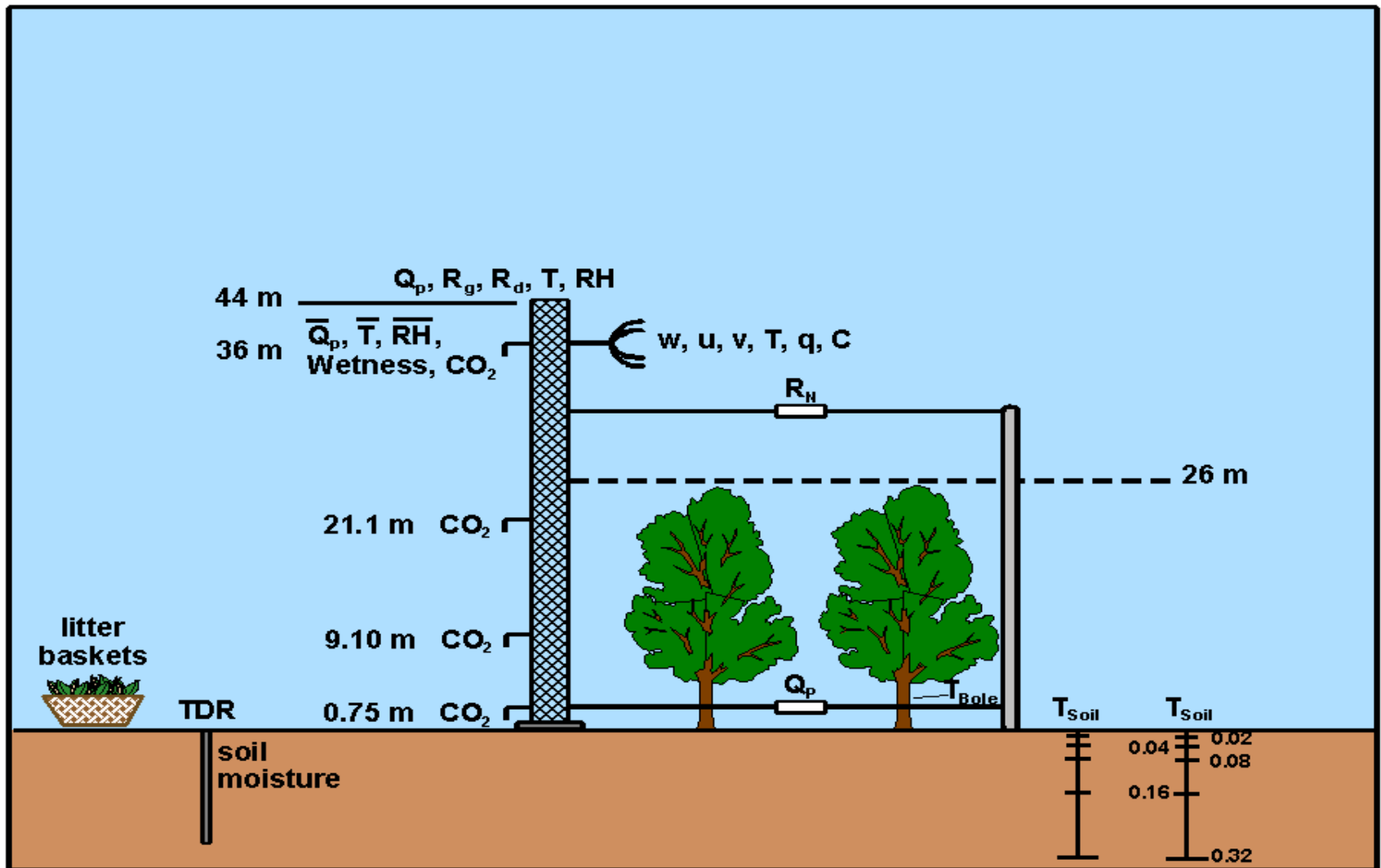
Global Carbon Cycle



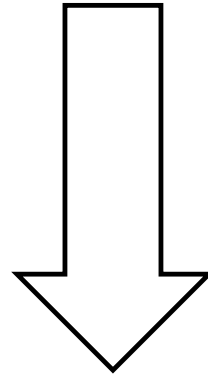
Ecology, Carbon Cycle



Typical setting for a flux station



ET or $NEE = f(\text{precipitation, temperature, soil moisture, } VPD, \text{ radiation, diffuse radiation, } LAI, \text{ vegetation type, etc.,})$



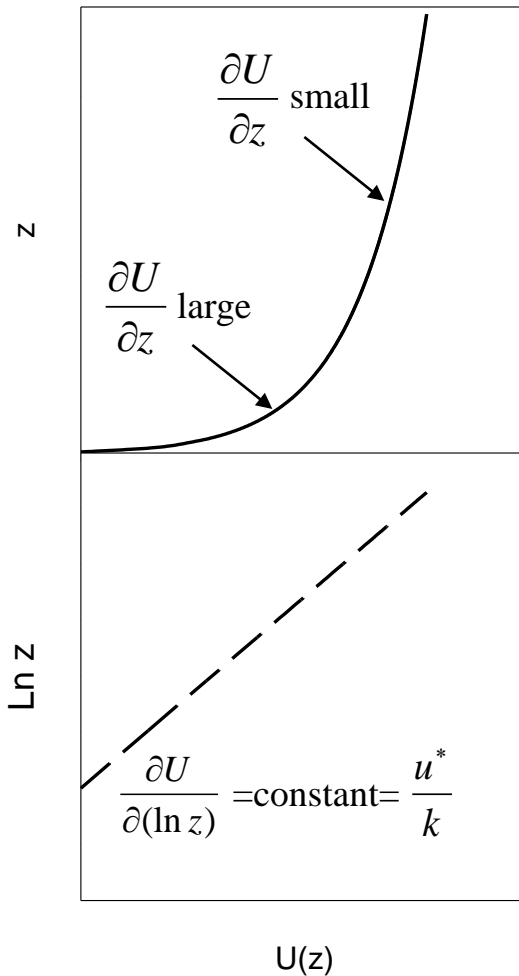
model validation, ground truth for remote sensing

Flux Footprint Concept For EC Experiment Design

Friction Velocity – u^*

Typical wind profile

Smooth surface and neutral stability



$$U_{(z)} = \frac{u^*}{k} \ln \frac{z}{z_0}$$

$U_{(z)}$ – horizontal wind speed at z

u^* - friction velocity $u^* = \sqrt{-\overline{u'w'}}$

k – von Karman constant (0.41)

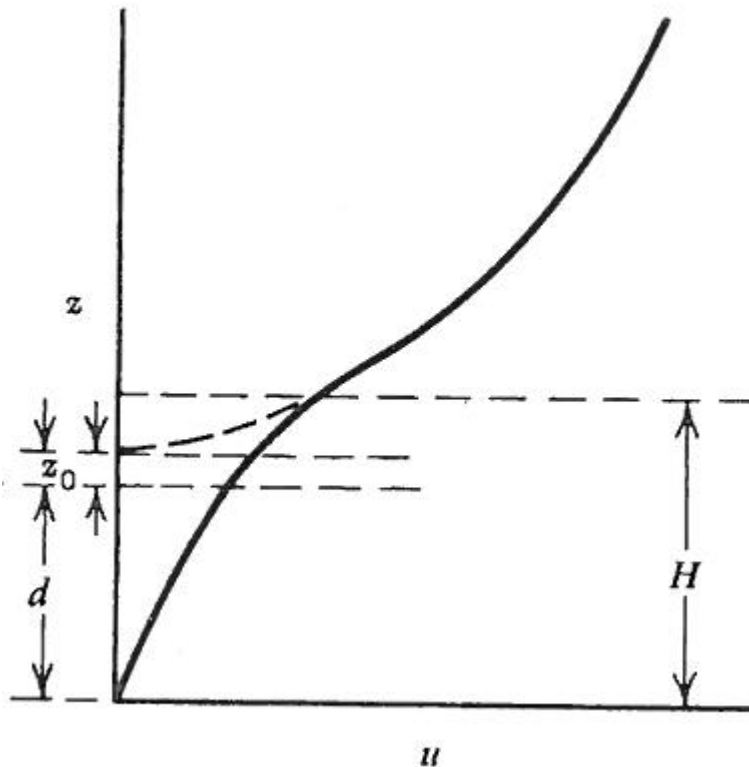
z – height

z_0 – roughness length

Friction Velocity – u^*

Typical wind profile

-Rough surface and neutral stability



$$U_{(z)} = \frac{u^*}{k} \ln \frac{z-d}{z_0}$$

$U_{(z)}$ – horizontal wind speed at z

u^* - friction velocity

k – von Karman constant (0.41)

z – height

z_0 – roughness length

d – zero plane displacement, ($d \approx 0.66 h$)

H – canopy height

Atmosphere Stability, Richardson number R_i

$$R_i = \frac{\frac{g}{\bar{\theta}} \frac{\partial \bar{\theta}}{\partial z}}{\left(\frac{\partial \bar{u}}{\partial z}\right)^2}$$

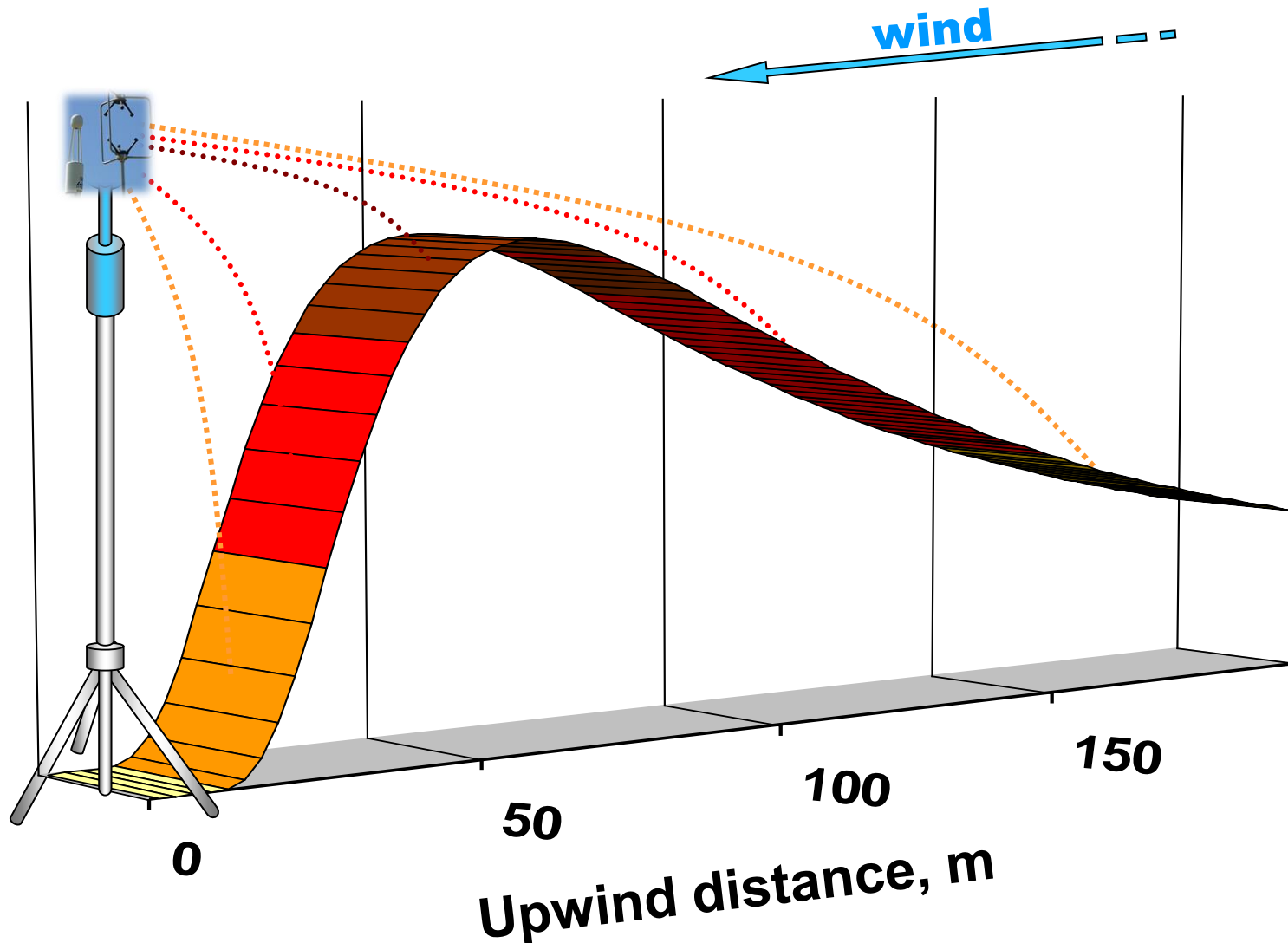
$\frac{\partial \bar{\theta}}{\partial z} > 0$	$R_i > 0$; stable
$\frac{\partial \bar{\theta}}{\partial z} = 0$	$R_i = 0$; neutral
$\frac{\partial \bar{\theta}}{\partial z} < 0$	$R_i < 0$; unstable

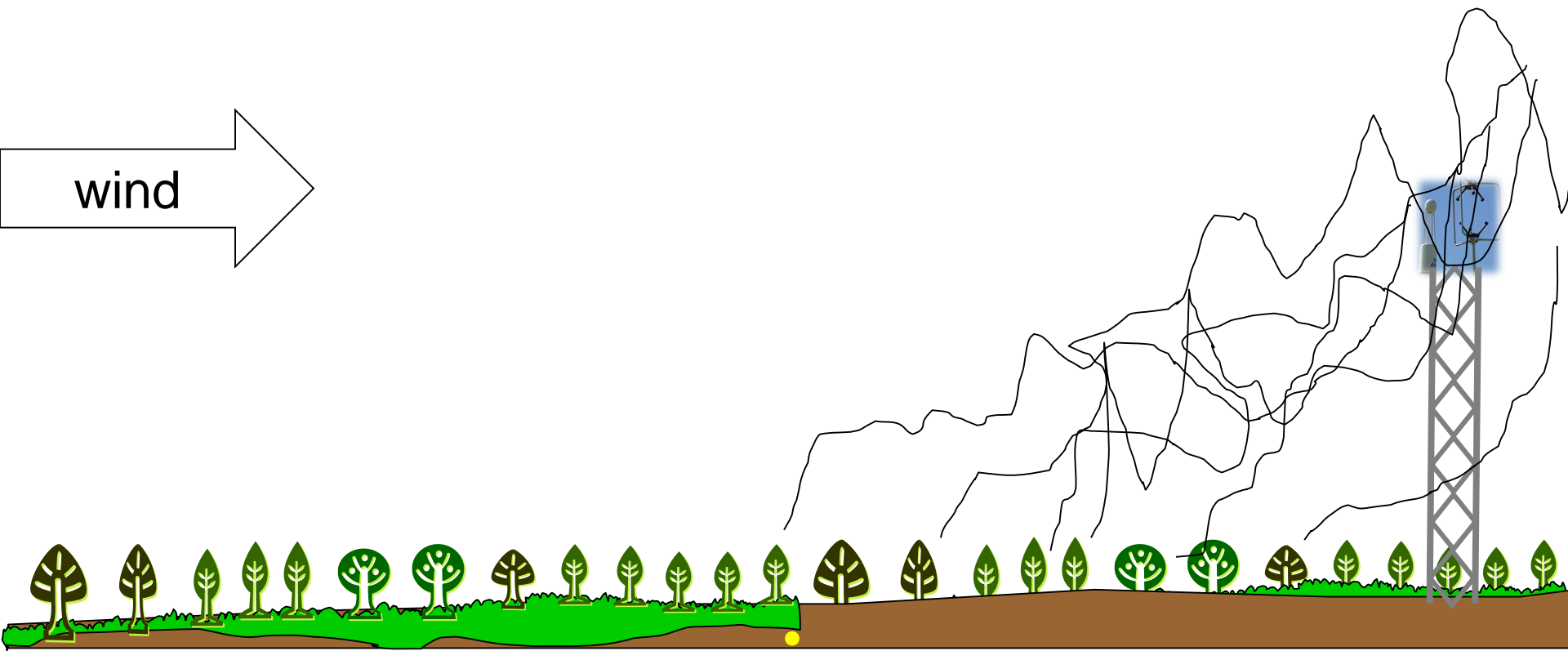
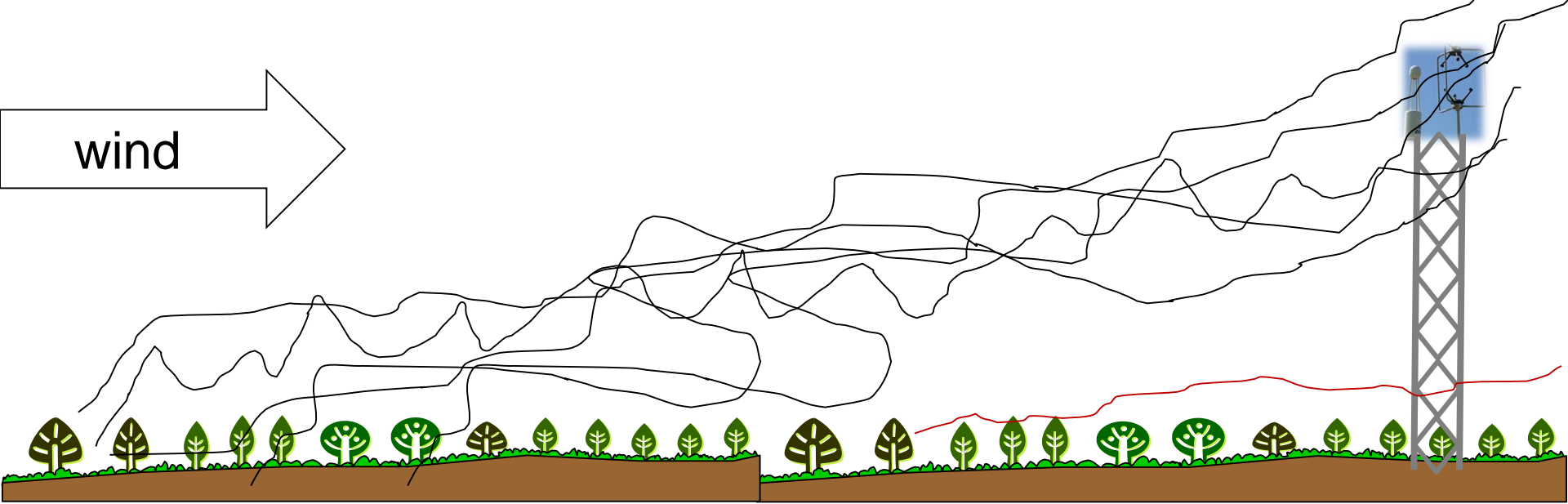
θ is potential temperature

Fetch Requirement

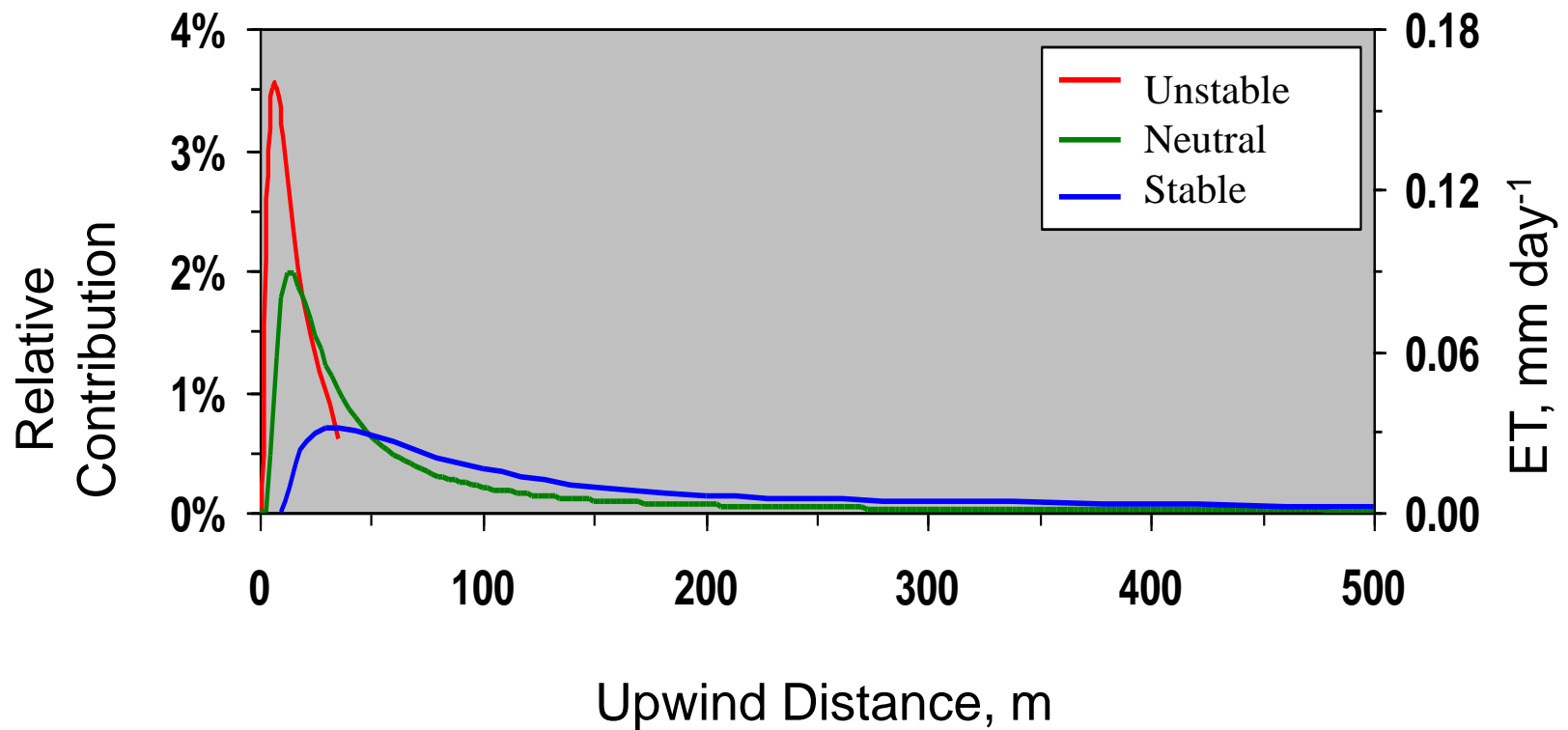


The footprint is defined as the relative contribution at different location (in the upwind direction) to the measured vertical flux





Instrument height 1.5 m, and canopy height 0.6 m





For near-neutral conditions:

$$CNF(x_L) = - \int_0^{x_L} \frac{U(z-d)}{u_* k x^2} e^{-\frac{U(z-d)}{u_* k x}} dx = e^{-\frac{U(z-d)}{u_* k x_L}}$$

CNF is Cumulative Normalized contribution to Flux measurement, %

x_L is distance from the tower, m

U is mean integrated wind speed, m s^{-1}

z is measurement height, m

u_* is friction velocity, m s^{-1}

$$U^* = \sqrt{-\overline{u'w'}}$$

d is zero plain displacement, m

k is von Karman constant (0.4)

Schuepp, P.H., Leclerc, M.Y., Macpherson, J.I., and R.L. Desjardins (1990)

'Footprint prediction of scalar fluxes from analytical solution of the diffusion equation'

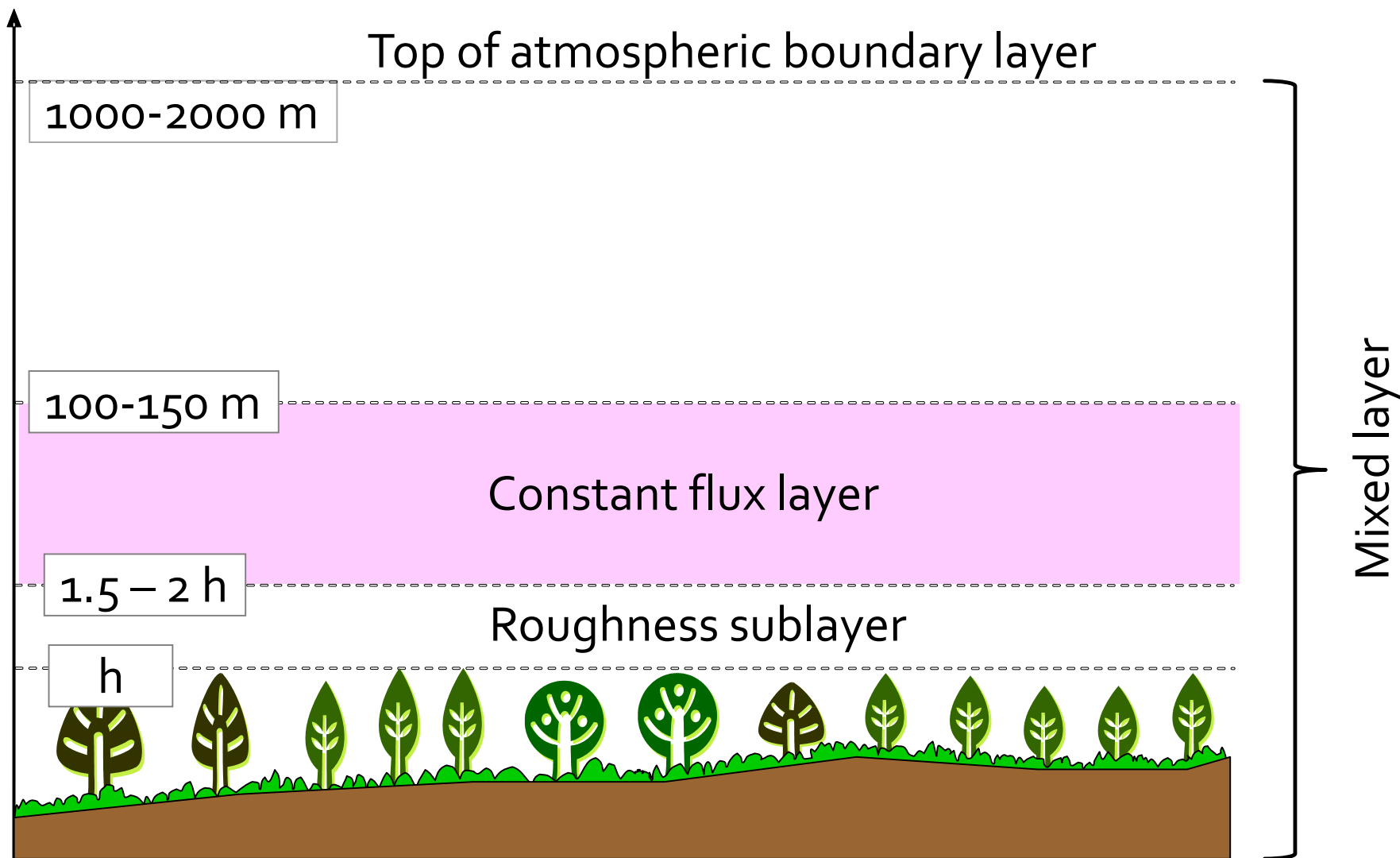
A grey arrow pointing to the right, with a small vertical bar at its tail.

Flux Footprint Depends on:

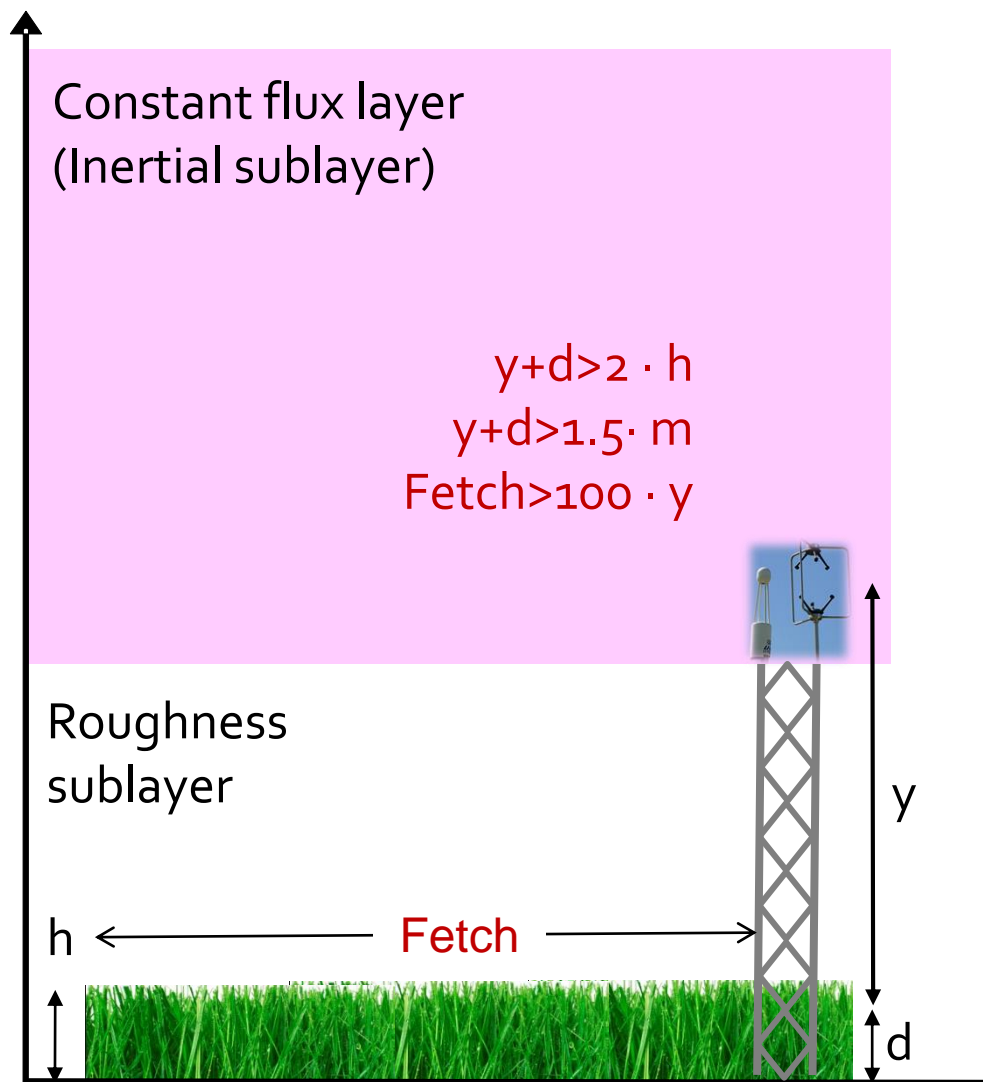
Measurement height

Mechanic mixing (dU/dz)

Thermal stability ($d\theta/dz$)



(layers are based on Stull, 1988; Denmead *et al.*, 1996; and Oke, 2007)

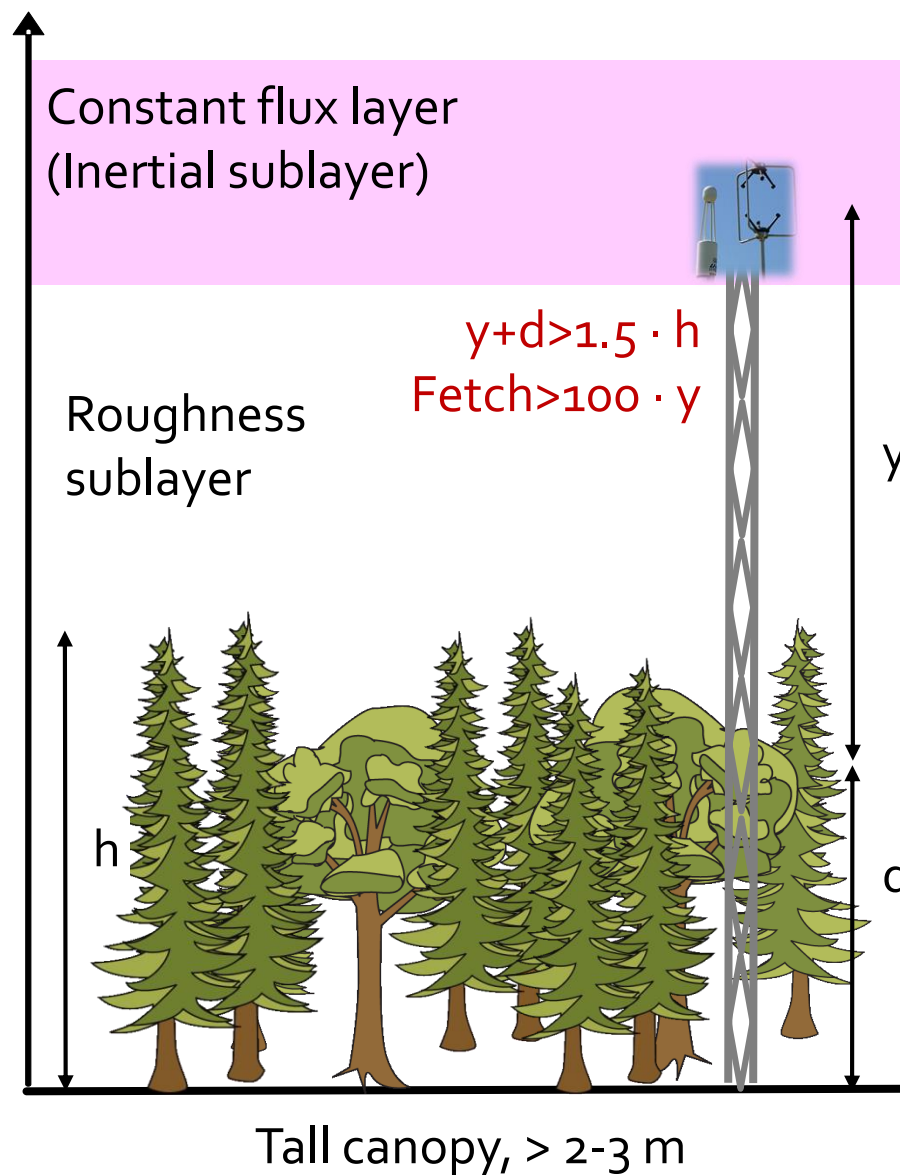


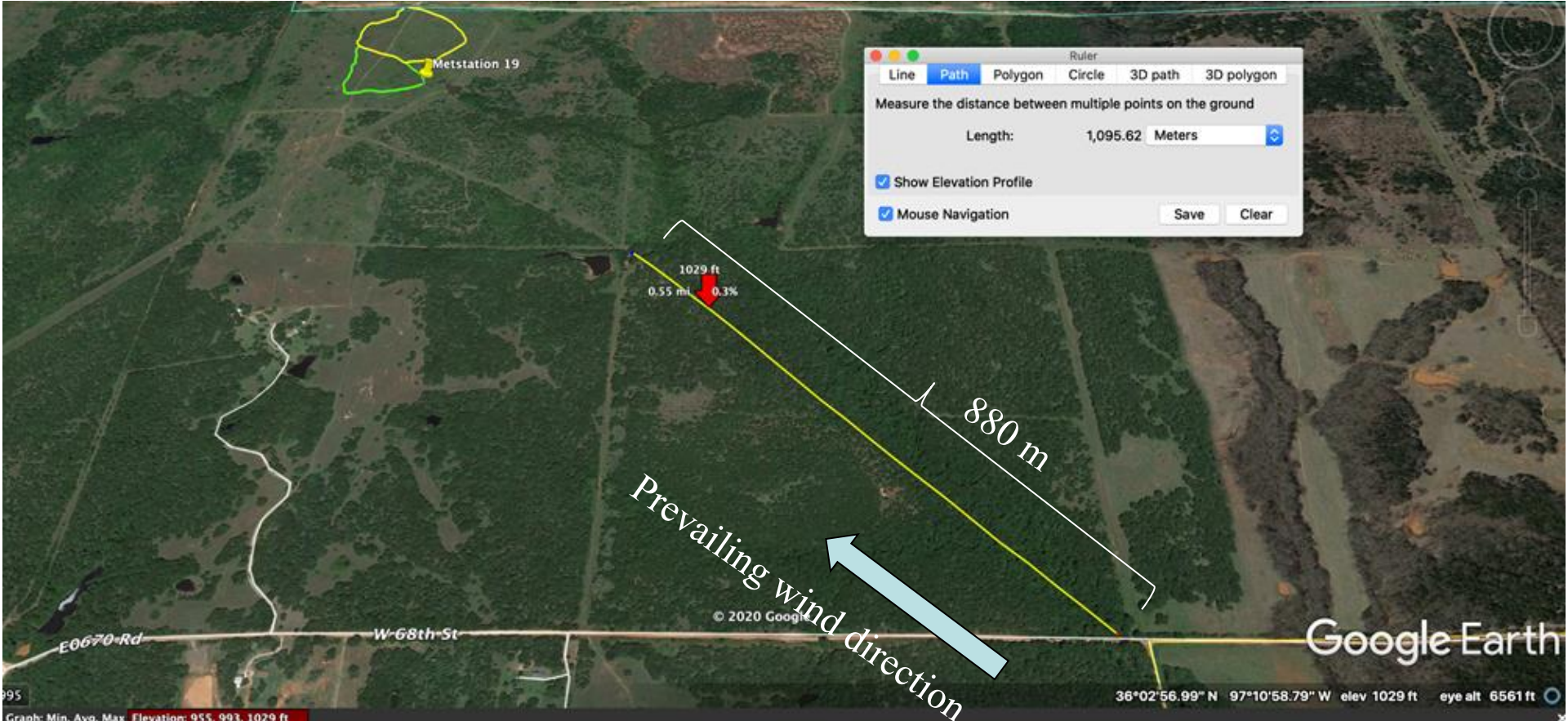
Short canopy, < 2-3 m

RULES OF THUMB



RULES OF THUMB





An example:

Criteria

$$y+d > 1.5 \cdot h$$

$$\text{Fetch} > 100 \cdot y$$

UIUC research site:

Canopy height: 8-10 m

Instrument height: 15 m

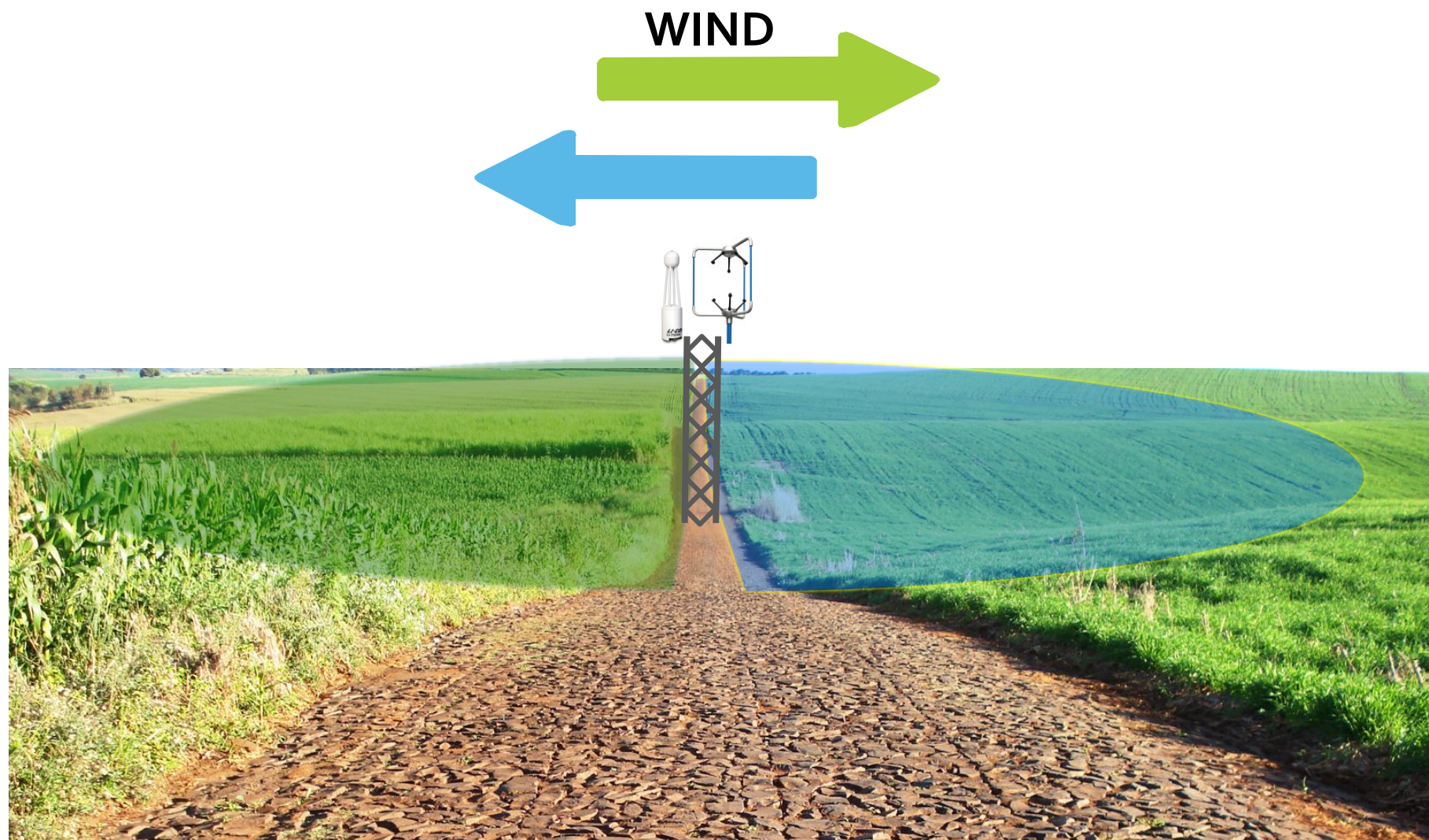
$$y-d = 15 - 6.8 = 8.2 \text{ m}$$

$$880 \text{ m} > 100 \times 8.2 \text{ m}$$

Tower Location



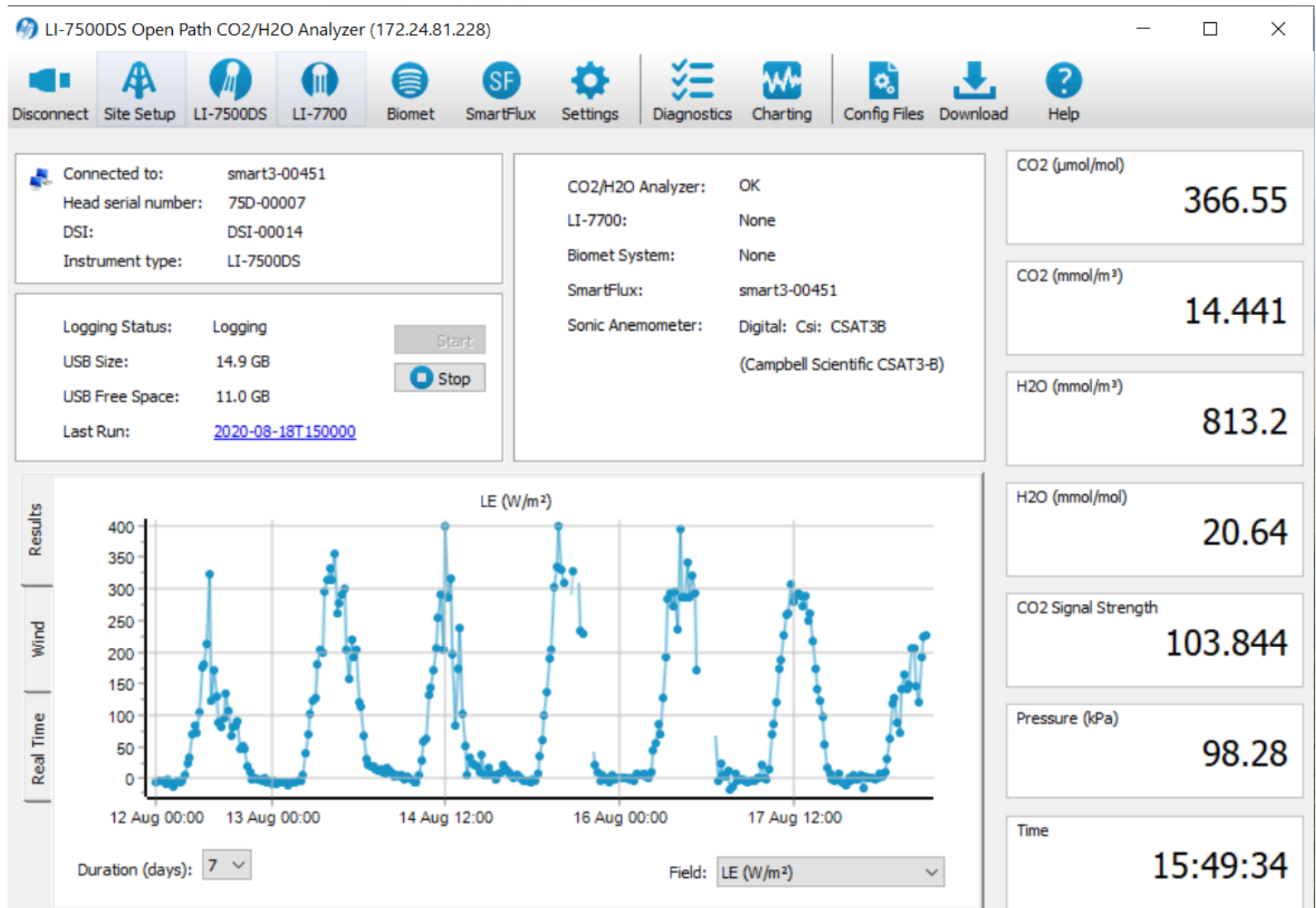
Tower Location?



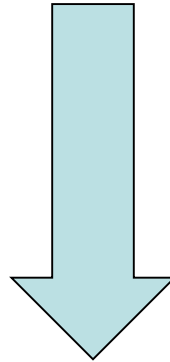
Daytime wind



Look through all channels to make sure output values in reasonable ranges?



Compute flux with EddyPro
as soon as you get back from the field



Do all the flux values make sense?
Do all the variables values make sense?

Analyze and look at
your data right away!

Summary

- Applications
- Footprint and fetch concept
- Tower location
- An important advices

Questions ?